APPENDIX G. Preliminary Civil Engineering and Drainage and Erosion Control Report

PRELIMINARY

CIVIL ENGINEERING AND DRAINAGE AND SOIL EROSION CONTROL REPORT

FOR

KAHOMA RESIDENTIAL SUBDIVISION

LAHAINA, MAUI, HAWAII

TAX MAP KEY: (2) 4-5-10:005

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OCTOBER 19, 2007

REVISED: DECEMBER 14, 2009 REVISED: OCTOBER 1, 2010 REVISED: NOVEMBER 8, 2010

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I. PURPOSE:

The purpose of this preliminary report is to investigate the infrastructure requirements for the proposed project. This report will present a brief description of the existing conditions and discuss anticipated improvements for roadway, drainage, water and sewer systems that are required by the appropriate governmental agencies.

II. PROPOSED PROJECT:

The proposed project involves the subdivision of a 16.683 acre property that is identified as Parcel 05 of Tax Map Key (2) 4-5-10. The conceptual subdivision layout is shown on Figure 8. It is subdivided into 76 lots that primarily include sixty eight (68) lots for single-family residences; one (1) for park use; one (1) for drainage pond; three (3) for access and utility purposes; and three (3) lots for roadway purposes. The single-family lots have areas ranging from 5,054 to 12,973 square feet.

Appurtenant to the proposed subdivision are grading, roadway, water, sewer and drainage systems that will be designed and constructed in accordance with the requirements of governmental agencies that review this type of development. The proposed improvements are discussed in their respective sections of this report.

III. LOCATION AND ACCESS:

A. <u>LOCATION</u>:

The project site is located in Lahaina, Maui, Hawaii. It is particularly situated on the southern side of Kahoma Stream Flood Control channel. Refer to Figures 1 and 2. Across the stream channel is Lahaina Business Park; while to the south of the proposed project are single-family residential subdivisions.

B. ACCESS:

Lui Street provides present access to the project site. This street joins Kalena Street which is in turn connected to Lahainaluna Road. Lahainaluna Road, which is the major access to the adjacent residential subdivisions, connects to Honoapiilani Highway that links West Maui to other parts of the island.

C. PROPOSED ROADWAY IMPROVEMENTS:

The future subdivision will be serviced internally by a 52-foot roadway that is planned to be privately owned and maintained. The upper (east) end will be connected to Lui Street, while the lower (west) end will tie into the existing old cane haul road that connects to Keawe Street. Refer to Figure 2. The existing road will be repaved to provide at least 20 feet wide pavement in compliance with Subsection 18.20.040B.3 of the Maui County Code.

A typical section of the proposed onsite roadway is shown on Figure 8. It includes a 6-foot wide concrete sidewalk along the northern side of the right-of-way; 9-foot wide planter on each side of the road; 4-foot wide bike lane along

each side of the 20-foot wide paved travelway; and concrete curbs. The proposed roadway will also include traffic calming features such as speed humps; signage; and pavement markings. It is also planned that parallel parking stalls (bubbled parking area) will be provided within the planter areas where space is available.

IV. EXISTING SOILS AND TOPOGRAPHY:

A. SOIL:

The U.S. Department of Agriculture Soil Conservation Service's <u>Soils Survey of the Island of Kauai, Oahu, Maui, Molokai and Lanai</u> [2], classifies the soils within the project site as Wahikuli Very Stony Silty Clay (WdB), 3 to 7 percent slopes and Rock Land (rRK) as shown on Figure 3. WdB, which occupies almost the entire site, is characterized as having moderate permeability, slow runoff and slight erosion hazard. It belongs to Wahikuli soil series that consist of well-drained soils on uplands on the island of Maui at elevations ranging from nearly sea level to 600 feet. These soils developed in material weathered from basic igneous rock.

rRK, which is found on the eastern tip of the project site, is made up of areas where exposed rock covers 25 to 90 percent of the land surface. This land type is nearly level to very steep.

B. <u>TOPOGRAPHY</u>:

The existing topography of the project site is shown on Figure 7.

The existing ground has elevations ranging from 32 feet to 145 feet above mean sea level. In general, the ground surface slopes down in a westerly direction from the east end to the west end of the project site, at an average slope of about 4½ percent.

1 A A

V. <u>WASTEWATER SYSTEM:</u>

A. <u>EXISTING</u>:

The existing wastewater system serving the adjacent residential subdivisions and nearby developments is part of the County's Lahaina Sewerage System. A portion of the system that collects wastewater flows generated by existing developments in the vicinity of the project site is shown on Figure 5. The collected wastewater is transmitted by a series of force mains and gravity sewerlines to the Lahaina Wastewater Reclamation Facility above the intersection of Honoapiilani Highway and Lower Honoapiilani Road, about 5 miles north of the project site.

B. PROJECTED WASTEWATER FLOW:

Based on the Wastewater Flow Standards [8], the estimated average wastewater flow generated by the proposed development is as follows:

Single-Family Residence = 68 lots x 350 gpd = 23,800 gallons per day

Total Average Wastewater Flow = 23,800 gallons per day

C. PROPOSED WASTEWATER SYSTEM:

The proposed wastewater system will consist of onsite and offsite systems. The onsite system is conceptually laid out on Figure 9; while the offsite system is schematically shown on Figure 5A.

The proposed onsite system will consist of 6" and 8" PVC sewer pipes and sewer manholes. Each proposed lot will be served by a single service lateral in compliance with the requirements of the Wastewater Reclamation Division (WWRD) of the Department of Environmental Management.

The proposed offsite system will consist of 8" PVC sewer pipes that will convey the project's wastewater flow to the existing 10-inch sewerline on Keawe Street as shown on Figure 5A. The offsite 8" sewerline will be laid out along the old cane haul road. An easement is needed from Kaanapali Land Management Corporation, who owns the old cane haul road. It may also require approval from the U.S. Army Corps of Engineers for crossing and/or anchoring the sewerline to the existing bridge over the Kahoma Stream Channel.

VI. WATER SYSTEM:

A. EXISTING:

There are existing waterlines that currently serve the existing developments in the vicinity of the project site. Refer to Figure 6. The system consists of water mains with sizes ranging from 2-inch to 12-inch pipes. The system that serves the residential subdivisions south of the project is fed by the existing 0.5 and 1.0 M.G. concrete water reservoirs on the upper reaches of Lahainaluna Road; while water for the existing developments across Kahoma Stream Channel

is supplied by the 1.5 MG Wahikuli storage tank which is located above Wahikuli Road.

B. PROJECTED WATER REQUIREMENTS:

1. <u>Domestic</u>:

According to Table 100-18, Domestic Consumption Guidelines, of the Department of Water Supply (DWS) Standards, the average daily domestic demand for single-family residences is 600 gallons per unit, respectively. Hence the average daily demand for the proposed project is as follows:

Single Family

= 68 x 600 gals./lot

= 40,800 gpd

Total Average Daily Demand

= 40,800 gpd

The maximum daily demand will be about 61,200 gpd which is 1.5 times the average daily demand (Table 100-20, Demand Factors).

2. Fire Flow:

The fire flow requirements (Table 100-19, Fire Flow Requirements) for the proposed single-family residential site is 1,000 gallons per minute (gpm). Fire hydrant will be at no more than 350 feet apart.

C. PROPOSED WATER SYSTEM IMPROVEMENTS:

With a relatively small residential development like this, the size of the distribution line is usually governed by the fire flow requirements. The needed

fire flow of 1,000 gpm for the single-family residential units will be used to size the main distribution line. Thus, an 8-inch waterline, which can deliver about 1,565 gpm at a velocity of 10 feet per second, is sufficient to provide the needed fire flow.

The conceptual water system is laid out on Figure 10. It consists of both onsite and offsite facilities. The onsite component includes 8-inch waterline, fire hydrants and service laterals. Individual single-family lots will be served by 5/8" water meters. The park site (Lot 70) will be served by a larger meter, tentatively 1½" meter, for both domestic and landscape watering purposes. Lot 69 which contains the drainage pond should also be provided with a water meter for irrigation. In keeping with the guidelines of the DWS Standards, the proposed fire hydrants will be spaced at no more than 350 feet apart.

Both ends of the onsite system will be tied-in to the existing waterline network serving the area. The upper end will be connected to the existing 8" and 4" waterlines at the intersection of Kahena and Kalena Streets through Lui Street. The lower end of the onsite system will be connected to the existing 12-inch waterline on Keawe Street via an 8-inch pipe across Kahoma Stream Channel and along the old cane haul road as shown on Figure 6. Similar with the offsite sewerline, this offsite waterline needs an easement from Kaanapali Land Management Corporation and may need approval by the U.S. Army Corps of Engineers.

VII. <u>DRAINAGE, GRADING AND SOIL EROSION</u>:

A. <u>GENERAL</u>:

The preliminary Drainage Study, in general, is based on the requirements, formulas, charts and tables of the Rules of the Design of Storm Drainage Facilities of the County of Maui [1] hereinafter referred to as County Drainage Standards; whereas, the Best Management Practices to control soil erosion are in accordance with the Construction Best Management Practices (BMPs) for the County of Maui [2] hereinafter referred to as "County Standard BMPs".

B. FLOODING HAZARD:

The site is found on Panels 0361E and 0362E map revised September 25, 2009, of the Flood Insurance Rate Map (FIRM) for the County of Maui. Refer to Figures 4 and 4A. The site is situated within Flood Designation Zone X where areas are subject to minimal flooding or areas determined to be outside the 0.2% annual chance flood plain. Therefore the proposed project does not need flood development permit as may be required by Chapter 19.62, Flood Hazard Areas, of the Maui County Code.

C. **EXISTING DRAINAGE CONDITIONS:**

The present onsite drainage flow pattern is generally characterized by sheet flow across the project site in a westerly direction discharging into Kahoma Stream channel at the upstream side of the existing cane haul bridge. The surface runoff enters the stream by flowing over the top of the concrete channel.

The site is part of the Kahoma Stream watershed.

D. STORM RUNOFF QUANTITIES:

Hydrologic calculations are given in Appendix A - Preliminary Drainage Calculations. According to the County Drainage Standards, the 10-year, 1-hour storm is used for design of surface drainage facilities such as roadway gutter flow, while the 50-year, 1-hour duration is used for the design of culverts and retention basins or drainage ponds.

Based on the preliminary drainage calculations (Appendix A), the overall project site is anticipated to increase the existing 1-hour rainfall storm as follows:

10-year Runoff Rate:

12.6 cfs, from 14.0 to 26.6 cfs

50-year Runoff Rate:

15.8 cfs, from 17.5 to 33.3 cfs

50-year Runoff Volume:

40,210 cf, from 44,675 to 84,885 cf

E. CONCEPTUAL DRAINAGE PLAN:

The drainage system scheme is laid out on Figure 11. The main feature of the proposed system is the construction of an onsite surface (open) retention basin or drainage pond that will be sized, at a minimum, to retain the 50-year, 1-hour storm runoff volume increase that is anticipated to be generated by the proposed project site. Storing the volume increase is expected to maintain the runoff volume leaving the project site below or at pre-development level.

Aside from the open-cut drainage pond, the proposed drainage system will also include catch basins and/or grated drain inlets to collect runoff; non-perforated pipes to convey runoff to the drainage pond; and drain manholes. It will also include the rerouting of the existing 30" and 36" drainlines between Lui Street and the Kahoma Stream Channel.

The proposed drainage pond will be constructed on Lot 69 as shown on Figure 11 while the conceptual grading plan is shown on Figure 12. The pond should be provided with the following:

- 1. Maintenance access where the side slopes are steeper than 4:1.
- A chainlink fence along the perimeter.
- Overflow spillway should the anticipated design storm is exceeded.
- 4. A freeboard of two (2) feet to provide a safety measure for the occurrence of a storm with intensity greater than the design storm.

F. GRADING REQUIREMENTS:

Grading for the proposed development will be performed in compliance with the applicable requirements of the Maui County Grading Ordinance. It is expected that grading will be essentially associated with the construction of the proposed roadways and developing building pads on each lot. This will involve grading almost the whole site that includes development of the drainage pond; cut and fill areas between the lots with minimum slopes at 2 horizontal to 1 vertical (2:1), if sufficient space is available; otherwise, grade adjustment walls will have to be constructed along the lot boundaries to obtain level surfaces for the future residential buildings especially on Lots 55 to 68.

A grading and grubbing permit must be obtained from the Development Services Administration (DSA) of the County of Maui prior to commencing land disturbance activities. Associated submittals for the permit application are Grading Plans, Soil Erosion Control Plan or Best Management Practices, Drainage Plan and Drainage Report.

G. <u>BEST MANAGEMENT PRACTICES</u>:

Requirements for the temporary control of soil erosion and dust during site improvement will be outlined and shown on the construction plans during the design development for the project. Some of the temporary control measures will be as follows:

- Installation of BMP such as silt fence, gravel bag berms or other approved sediment trapping devices at the downstream side of the grading area and sediment pits.
- 2. Installation of dust control fence surrounding the project site.
- Control dust by means of water trucks or by installing temporary sprinkler systems or both if necessary.
- Graded areas shall be thoroughly watered after construction activity has ceased for the day and for weekends and holidays.
- All exposed areas shall be paved, grassed, or permanently landscaped as soon as finished grading is completed.
- 6. Storm runoff will be diverted away from graded areas to natural drainageways during construction by means of sand bag berms or lined temporary swales.
- 7. Time of construction will be minimized.
- 8. Only areas that are needed for new improvements will be cleared.
- 9. Early construction of drainage control features.
- Construction of pit for proposed drainage ponds prior to mass grading of project site. The pits will be temporarily utilized as sediment catchment during construction.

11. Temporary control measures shall be in place and functional prior to construction and shall remain operational throughout the construction period or until permanent controls are in place.

The Contractor will also be required to submit a satisfactory soil erosion control plan to minimize soil erosion prior to an issuance of a grubbing and grading permit. Best Management Practices shall be in compliance with Section 20.08.035 of the Maui County Code (Ord. No. 2684) and County Standard BMPs.

The grading area is expected to be larger than 1.0 acre. Hence, NPDES General Permit Coverage Authorizing Discharges of Storm Water associated with construction activities will need to be obtained from the State Department of Health, Clean Water Branch, prior to any land disturbance at the project site.

H. CONCLUSION:

Based on this preliminary drainage study, the proposed development will increase the existing storm runoff due to addition of impervious surfaces such as building roofs, pavement and concrete walkways. Despite the increase in runoff, the proposed development is not anticipated to have adverse drainage effects on adjacent and downstream properties. In keeping with the guidelines of the County Drainage Standards, the proposed drainage improvements will include the impoundment of the 50-year, 1-hour storm runoff volume increase to be generated by the future development. The future onsite drainage pond will result in a zero runoff increase for the 50-year storm to downstream properties and will also have the effect of reducing the potential for sediments contained in the runoff from entering the ocean.

Soil erosion and dust control measures (BMPs) will be instituted during development of the proposed project. These measures will include BMPs in compliance with County Standard BMPs and Section 20.08.035 of the Maui County Code. Additionally, NPDES General Permit Coverage Authorizing Discharge of Storm Water Associated with Construction Activities will be obtained from the Clean Water Branch of the State Department of Health prior to any land disturbance. Conditions of the permit will be implemented during site construction.

IX. CONSTRUCTION PLAN APPROVALS:

Approval of construction plans and appropriate permits for site grading and infrastructural improvements of the proposed project will be obtained from the Department of Public Works; Department of Environmental Management; Department of Water Supply; Fire Prevention Bureau; State Department of Health, Wastewater and Clean Water Branches; and the U.S. Army Corps of Engineers. The various infrastructures will be designed in compliance with the applicable requirements of these governmental agencies.

X. <u>REFERENCES</u>:

- 1. Rules for the Design of Storm Drainage Facilities in the County of Maui,
 Title MC-15, Department of Public Works and Waste Management,
 County of Maui, Chapter 4.
- Construction Best Management Practices (BMPs) for the County of Maui, Department of Public Works and Waste Management, May 2001.
- Soil Survey of Islands of Kauai, Oahu, Maui, Molokai and Lanai, State of Hawaii, prepared by U. S. Department of Agriculture, Soil Conservation Service, August 1972.

- 4. <u>Erosion and Sediment Control Guide for Hawaii</u>, prepared by U. S. Department of Agriculture, Soil Conservation Service, March 1981.
- 5. Rainfall-Frequency Atlas of the Hawaiian Islands, Technical Paper No. 43, U. S. Department of Commerce, Weather Bureau, 1962.
- 6. Flood Insurance Rate Maps for the County of Maui
- 7. <u>Water System Standards</u>, Department of Water Supply, County of Maui, 2002.
- 8. <u>Wastewater Flow Standards</u>, Wastewater Reclamation Division, Department of Public Works & Environmental Management, February 2, 2000.

APPENDIX A

KAHOMA RESIDENTIAL SUBDIVISION LAHAINA, MAUI, HAWAII TMK: (2) 4-5-10:005

PRELIMINARY DRAINAGE CALCULATIONS

December 2009 Revised: October 1, 2010 Revised: November 8, 2010

I. <u>Reference</u>: Rules for the Design of Storm Drainage Facilities in the County of Maui, April 14, 1995

U. B. To determine the executions and next develop

II. <u>Purpose</u>: To determine the overall pre and post development storm runoff discharges.

III. <u>Hydrologic Criteria</u>:

A. 10-Year, 1-Hour: for design of surface facilities such as gutter

1-Hr. Rainfall Value = 2.0"

B. 50-Year, 1-Hour: for design of retention ponds and roadway culverts

1-Hr. Rainfall Value = 2.5"

IV. Runoff Quantity:

- A. Runoff Discharge Rate & Volume:
 - 1. <u>Methodology</u>:

Rational Method, Q = CIA

Where Q = Flow rate in cubic feet per second (cfs)

C = Runoff Coefficient

 Rainfall intensity in inches per hour for a duration equal to the time of concentration

A = Drainage Area in Acres (See Figure 13)

Calculations employing this method were performed on computer using hydrologic software "Hydraflow Hydrographs 2004" by Intelisolve. The Standard Rational Method is used to calculate storm runoff peak discharge rates while the Modified Rational Method is employed to determine storm runoff volumes. The intensity duration frequency (IDF) curves were developed by inputting into the program the intensity values for 5, 15, 30 and 60 minutes duration corresponding to the 10-year and 50-year, 1-hour rainfall amounts as determined from Plate 2.

2. Runoff Coefficient, C:

Existing Condition:

C = 0.30 (Unimproved)

Future Condition:

C = 0.55 (Residential)

= 0.80 (Roadway)

= 0.22 (Park/Open Space)

Determine weighted runoff coefficient, C_{W} , of project site at developed conditions:

$$C_{W} = \frac{A_{1} \times C_{1} + A_{2} \times C_{2} + A_{3} \times C_{3}}{A_{1} + A_{2} + A_{3}}$$

Where:

 $A_1 = 12.21$ Acs. (Residential)

 $A_2 = 3.23$ Acs. (Roadway)

 A_3 = 1.44 Acs. (Open Space/Park)

$$C_{w} = \frac{12.21 \times 0.55 + 3.23 \times 0.80 + 1.44 \times 0.22}{16.88}$$

$$= \frac{9.616}{16.88}$$

$$= 0.57$$

3. <u>Time of Concentration, Tc</u>:

Length of Flow = 2,600 ft.

Average Slope = 4.5%

Tc = 30 min. (Poor Grass)

4. Storm Runoff Quantity:

(Refer to attached Hydrograph Report)

1-Hour Storm Peak Discharge Rate:

	Existing	<u>Future</u>	<u>Increase</u>
10-Year	= 14.0 cfs	= 26.6 cfs	= 12.6 cfs
50-Year	= 17.5 cfs	= 33.3 cfs	= 15.8 cfs

5. Runoff Volume (50-Year, 1-Hour Storm):

(Refer to attached Hydrograph Report)

<u>Existing</u> <u>Future</u> <u>Increase</u>
= 44,675 cf = 84,885 cf = 40,210 cf

The 50-year, 1-hour rainfall volume increase is the minimum volume to be retained onsite in order to attain zero runoff increase to adjacent/downstream properties.

V. Retention Pond:

In accordance with the County Drainage Standards, retention pond shall have a storage capacity to at least equal to the anticipated 50-year, 1-hour storm runoff volume increase for drainage areas less than 100 acres; however, in determining the storage capacity, soil percolation shall not be taken into account. Based on this guideline, the proposed project will require a minimum storage of 40,210 cf.

The conceptual grading plan of the proposed drainage pond is shown on Figure 12. Storage capacity of the proposed pond is given in the attached "Pond Report". Allowing for a freeboard of 2 feet; the design capacity of the proposed pond is about 46,510 cf resulting in an excess of 6,300 cf over the volume increase.

Pond Report

Hydraflow Hydrographs by Intelisolve

Thursday, Nov 4 2010, 3:39 PM

Pond No. 3 - Proposed Drainage Pond

Pond Data

Bottom LxW = 95.0×60.0 ft

Side slope = 2.0:1

Bottom elev. = 0.00 ft

Depth = 8.00 ft

Stage	1	Storage	Table
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Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuf	ft)
0.00	0.00	5,700	0	0	
0.40	0.40	5,951	2,330	2,330	
0.80	0.80	6,206	2,431	4,761	
1.20	1.20	6,467	2,534	7,296	
1.60	1.60	6,733	2,640	9,935	
2.00	2.00	7,004	2,747	12,683	
2.40	2.40	7,280	2,857	15,539	
2.80	2.80	7,561	2,968	18,507	
3.20	3.20	7,848	3,082	21,589	
3.60	3.60	8,139	3,197	24,786	
4.00	4.00	8,436	3,315	28,101	
4.40	4.40	8,738	3,435	31,536	
4.80	4.80	9,045	3,556	35,092	
5.20	5.20	9,357	3,680	38,772	
5.60	5.60	9,674	3,806	42,578	P. @2 FB & 46,510 CF
6.00	6.00	9,996	3,934	70,012	F. 6 4 F. 6 4 40,000
6.40	6.40	10,323	4,064	50,576	
6.80	6.80	10,656	4,196	54,771	
7.20	7.20	10,993	4,330	59,101	
7.60	7.60	11,336	4,466	63,567	
8.00	8.00	11,684	4,604	68,171	

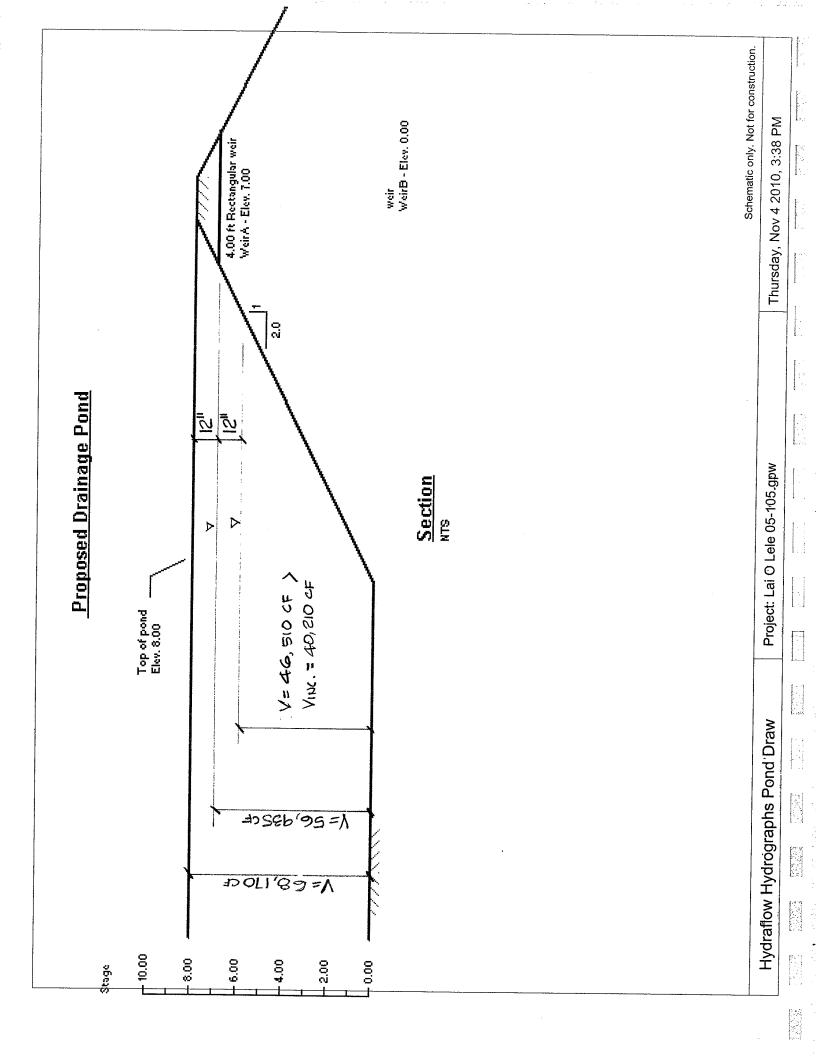
Culvert / Orifice Structures

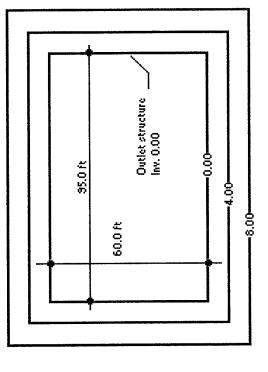
Weir Structures

	[A]	[B]	[C]	[D]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 4.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 7.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	0.00	0.00	0.00
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	= Rect			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	0.00	_				
N-Value	= .000	.000	.000	.000					
Orif. Coeff.	= 0.00	0.00	0.00	0.00					
Multi-Stage	= n/a	No	No	No	Exfiltration = (0.000 in/hr (W	'et area) T	ailwater E	lev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table												
Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	Clv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
0.00	0	0.00					0.00		***			0.00
0.40	2,330	0.40					0.00					0.00
0.80	4,761	0.80					0.00					0.00
1.20	7,296	1.20					0.00					0.00
1.60	9,935	1.60					0.00					0.00
2.00	12,683	2.00					0.00					0.00
2.40	15,539	2.40					0.00					0.00
2.80	18,507	2.80					0.00					0.00
3.20	21,589	3.20					0.00					0.00
3.60	24,786	3.60					0.00					0.00
4.00	28,101	4.00					0.00					0.00
4.40	31,536	4.40					0.00					0.00
4.80	35,092	4.80					0.00					0.00
5.20	38,772	5.20					0.00					0.00
5.60	42,578	5.60					0.00					0.00
6.00	46,512	6.00					0.00					0.00
6.40	50,576	6.40					0.00					0.00
6.80	54,771	6.80					0.00					0.00
7.20	59,101	7.20					1.19					1.19
7.60	63,567	7.60					6.19					6.19
8.00	68,171	8.00					13.32					13.32





Plan View NTS Schematic only. Not for construction.

Thursday, Nov 4 2010, 3:39 PM

Project: Lai O Lele 05-105.gpw

Hydraflow Hydrographs by Intelisolve

Wednesday, Oct 27 2010, 2:50 PM

Hyd. No. 11

Overall runoff rate (existing)

Hydrograph type = Rational Storm frequency = 10 yrs Drainage area = 16.680 ac

Intensity = 2.800 in/hr

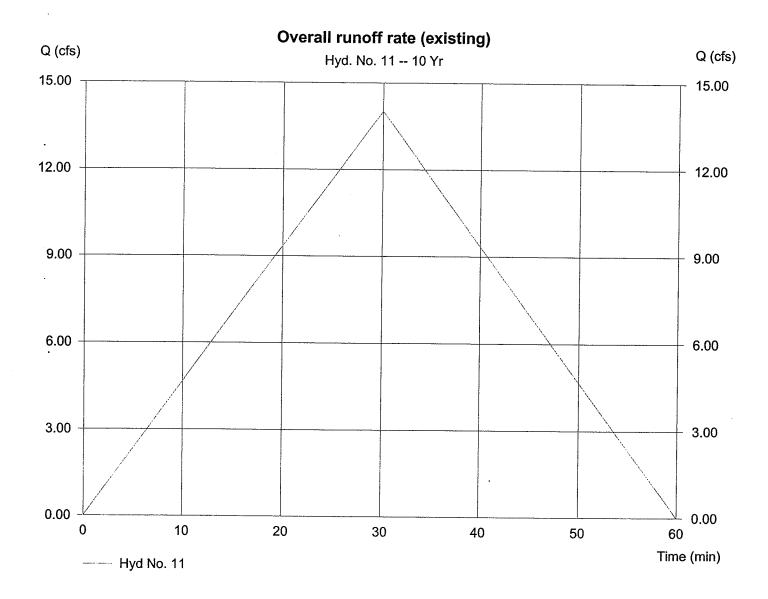
IDF Curve = Lai O Lele 05-105.IDF

Peak discharge = 14.01 cfs Time interval = 1 min Runoff coeff. = 0.3

Tc by User = 30.00 min

Asc/Rec limb fact = 1/1

Hydrograph Volume = 25,220 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Wednesday, Oct 27 2010, 2:50 PM

Hyd. No. 11

Overall runoff rate (existing)

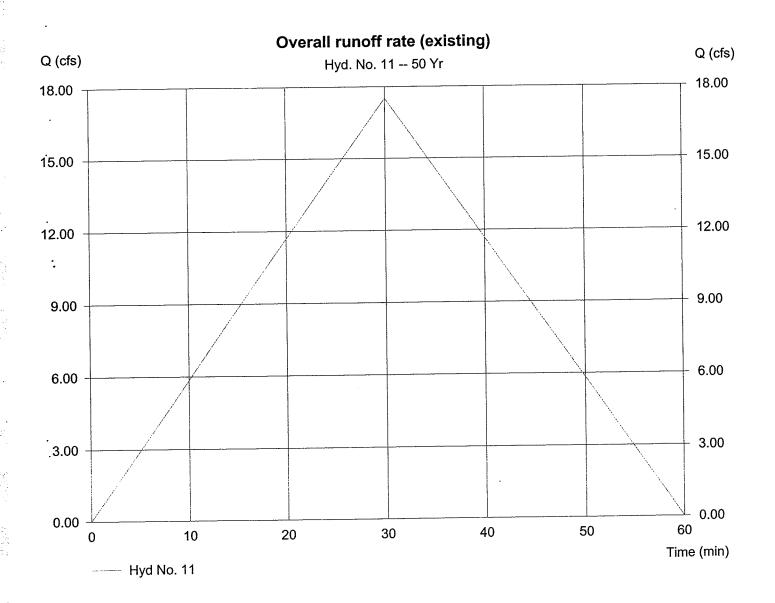
Hydrograph type = Rational Storm frequency = 50 yrs Drainage area = 16.680 ac

Intensity = 3.500 in/hr

IDF Curve = Lai O Lele 05-105.IDF

Peak discharge = 17.51 cfs
Time interval = 1 min
Runoff coeff. = 0.3
Tc by User = 30.00 min
Asc/Rec limb fact = 1/1

Hydrograph Volume = 31,525 cuft



Hydraflow Hydrographs by Intelisolve

Wednesday, Oct 27 2010, 2:50 PM

1

Hyd. No. 12

Overall runoff rate (future)

Hydrograph type = Rational Storm frequency = 10 yrs Drainage area = 16.680 ac

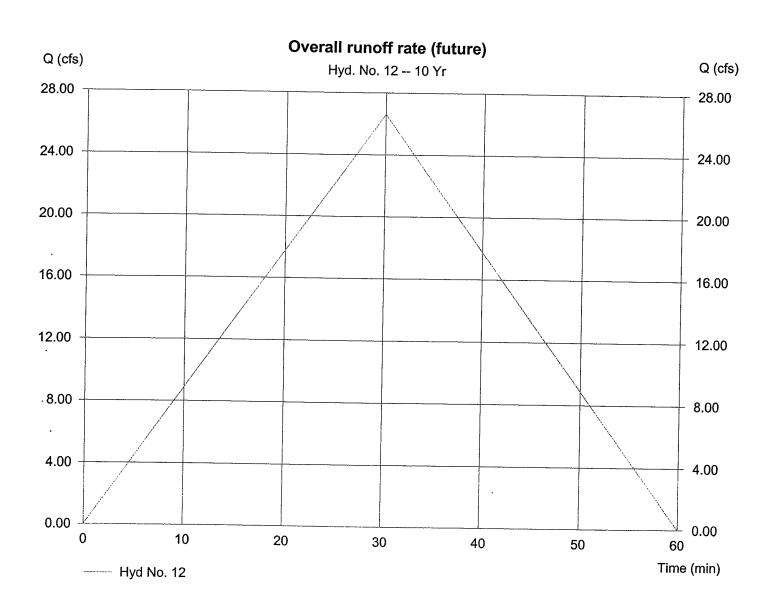
Intensity = 2.800 in/hr

IDF Curve = Lai O Lele 05-105.IDF

Peak discharge = 26.62 cfs Time interval = 1 min Runoff coeff. = 0.57 Tc by User = 30.00 min

Asc/Rec limb fact = 1/1

Hydrograph Volume = 47,918 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisoive

Wednesday, Oct 27 2010, 2:50 PM

Hyd. No. 12

Overall runoff rate (future)

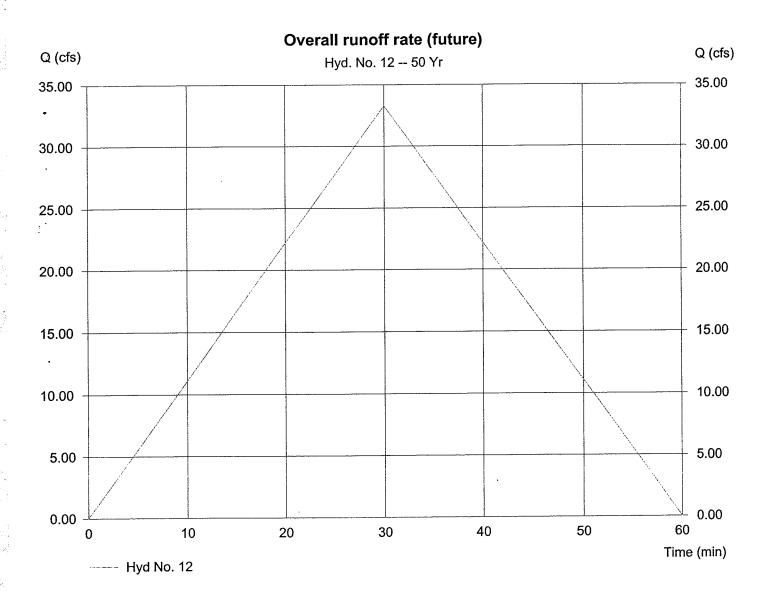
Hydrograph type = Rational Storm frequency = 50 yrsDrainage area = 16.680 ac

Intensity **IDF** Curve

= 3.500 in/hr= Lai O Lele 05-105.IDF Peak discharge = 33.28 cfsTime interval = 1 min Runoff coeff. = 0.57Tc by User = 30.00 min

Asc/Rec limb fact = 1/1

Hydrograph Volume = 59,898 cuft



Hyd. No. 13

Overall runoff volume (existing)

Hydrograph type = Mod. Rational

Storm frequency = 50 yrsDrainage area = 16.680 acIntensity

IDF Curve

= 2.480 in/hr

= Lai O Lele 05-105.IDF

Peak discharge

= 12.41 cfs

Time interval

= 1 min

Runoff coeff.

Tc by User

= 0.3

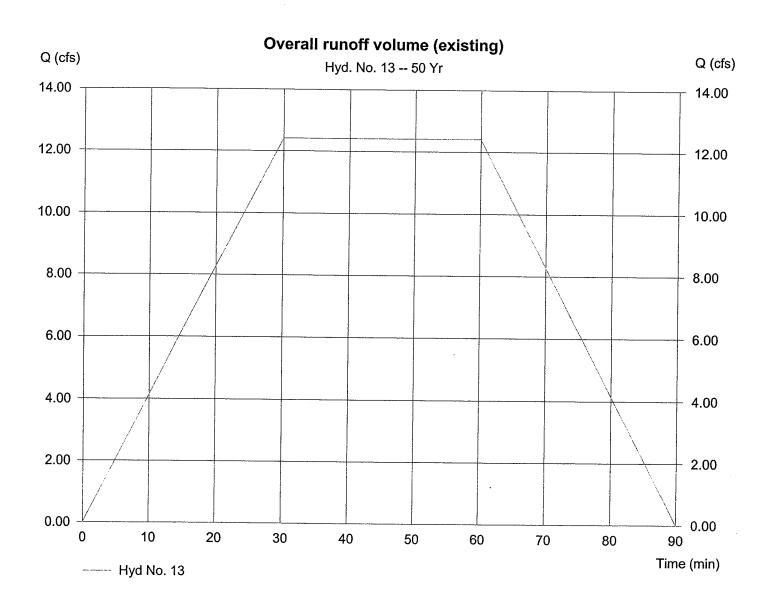
Storm duration

= 30.00 min $= 2 \times Tc$

Hydrograph Volume = 44,676 cuft

≈ 44,675 CF

1



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Wednesday, Oct 27 2010, 2:51 PM

Hyd. No. 14

Overall runoff vloume (future)

Hydrograph type = Mod. Rational

Storm frequency = 50 yrs Drainage area = 16.680 ac Intensity = 2.480 in/hr

IDF Curve = Lai O Lele 05-105.IDF

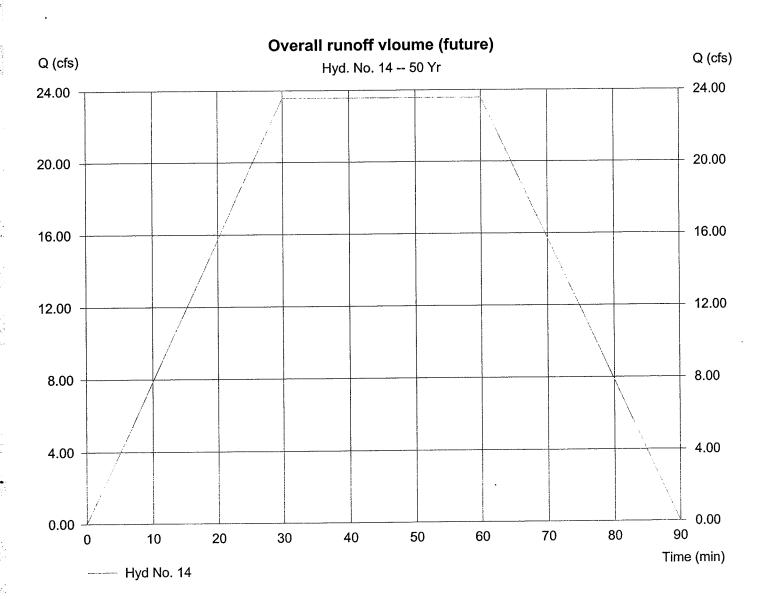
Peak discharge = 23.58 cfs
Time interval = 1 min

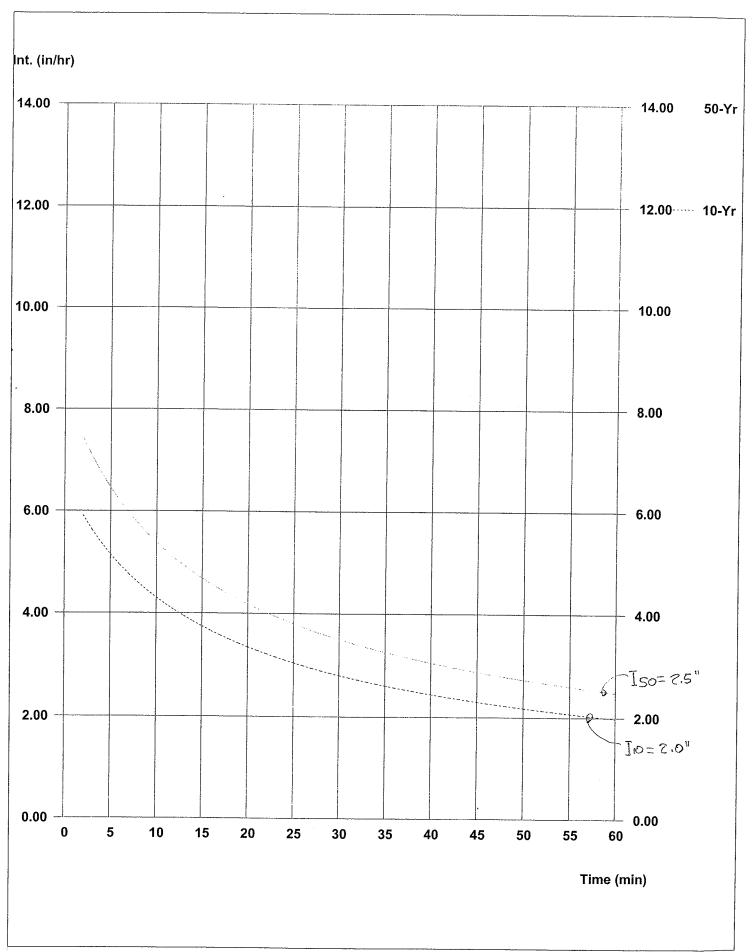
Runoff coeff. = 0.57 Tc by User = 30.00 min

Storm duration = $2 \times Tc$

Hydrograph Volume = 84,884 cuft

≈ 84,885 cf





Hydraflow IDF Report

Return Period	Equation Coefficients (FHA)								
(Yrs)	В	D	E	(N/A)					
1	0.0000	0.0000	0.0000						
2	0.0000	0.0000	0.0000						
3	0.0000	0.0000	0.0000						
5	0.0000	0.0000	0.0000						
10	27.3279	9.9000	0.6180						
25	0.0000	0.0000	0.0000						
50	32.9258	9.5000	0.6097						
100	0.0000	0.0000	0.0000						
	well-barberstoneklivdezveranda	s 2004\trai O Lele 05-105.fC	F						

Intensity = $B / (Tc + D)^{A}$

Return												0.49
Period (Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	5.15	4.30	3.75	3.35	3.04	2.80	2.60	2.44	2.30	2.18	2.07	1.98
25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
50	6.45	5.38	4.68	4.18	3.80	3.50	3.25	3.05	2.88	2.73	2.60	2.48
100	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
c = time in m												

GUIDE FOR THE DETERMINATION OF RUNOFF COEFFICIENTS FOR BUILT-UP ARE AS*

WATERSHED CHARACTERISTICS	EXTREME	нівн	MODERATE	LOW
INFILTRATION	NEGLIGIBLE 0,20	SLOW 0.14	MEDIUM 0.07	HIGH 0.0
RELIEF	STEEP (> 25%)	HILLY (15 - 25%)	ROLL(NG (5-15%)	FLAT (0-5%)
	0.08	0.06	0.03	0.0
VEGETAL	NONE	POOR (< 10%)	GOOD (10-50%)	HIGH (50-90%)
COVER	0.07	0.05	0.03	0.0
DEVELOPMENT TYPE	INDUSTRIAL & BUSINESS 0.55	HOTEL - APARTMENT 0.45	RESIDENTIAL 0.40	AGRICULTURAL 0.15 ,

^{*}NOTE: The design coefficient "c" must result from a total of the values for all four watershed characteristics of the site.

Table 2

RUNOFF COEFFICIENTS

Type of Drainage Area	Runoff Coefficient C
Parks, cemeteries	0.25
Playgrounds	0.35
Railroad yard areas	0.40
Unimproved areas	0.30
Streets:	
Asphaltic	0.95
Concrete	0.95
Brick	0.85
Driveway and walks	0.85
Roofs	0.95
Lawns:	
Sandy soil, flat, 2%	0.10
Sandy soil, avg., 2-7%	0.15
Sandy soil, steep, 7%	0.20
Heavy soil, flat, 2%	0.17
Heavy soil, avg., 2-7%	0.22
Heavy soil, steep, 7%	0.35

MINIMUM RUNOFF COEFFICIENTS FOR BUILT-UP AREAS

Residential areas	C=0.55
Hotel, apartment areas	C=0.70
Business areas	C=0.80
Industrial areas	C=0.80

The type of soil, the type of open space and ground cover and the slope of the ground shall be considered in arriving at reasonable and acceptable runoff coefficients.

Table 4

APPROXIMATE AVERAGE VELOCITIES OF RUNOFF FOR CALCULATING TIME OF CONCENTRATION

TYPE OF FLOW	VELOCITY IN FPS FOR SLOPES (in percent) INDICATED					
OVERLAND FLOW: Woodlands Pastures Cultivated Pavements	0-3% 1.0 1.5 2.0 5.0	4-7% 2.0 3.0 4.0 12.0	8-11% 3.0 4.0 5.0 15.0	12-15% 3.5 4.5 6.0 18.0		
OPEN CHANNEL FLOW: Improved Channels Natural Channel* (not well defined)	Determin	ne Velocit 3.0	y by Mainin 5.0	g's Formula 8.0		

*These values vary with the channel size and other conditions so that the ones given are the averages of a wide range. Wherever possible, more accurate determinations should be made for particular conditions by Manning's formula.

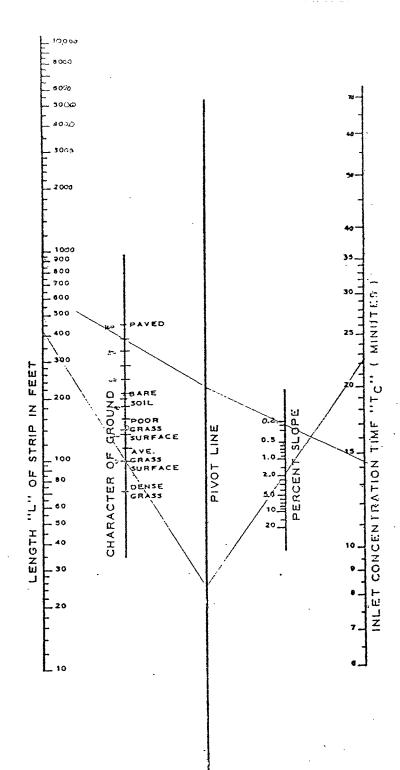
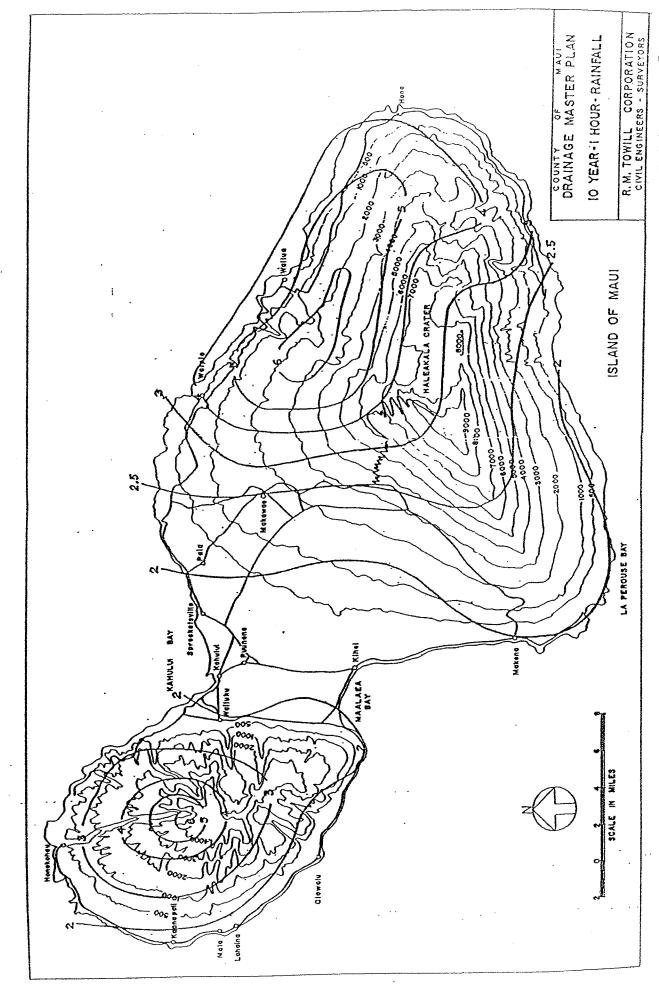
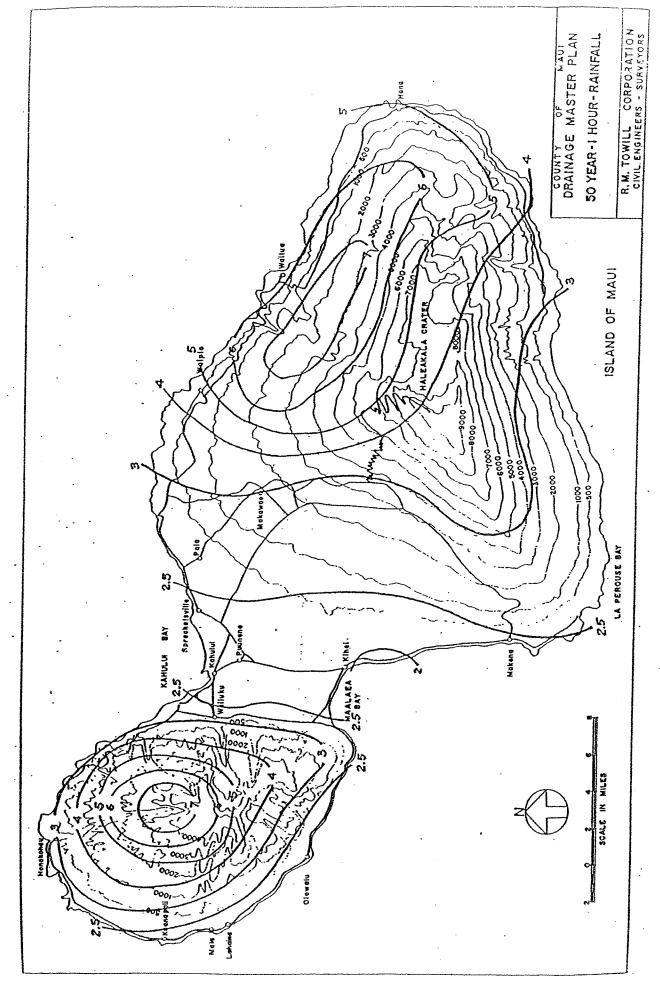
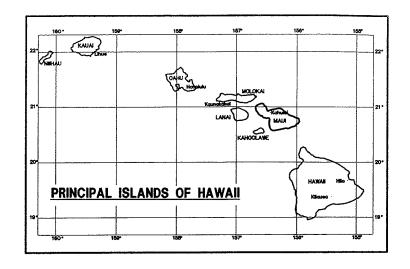


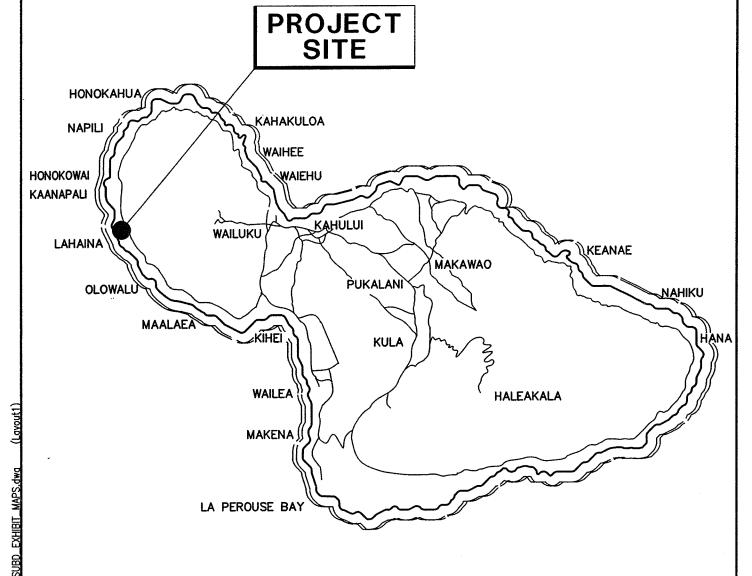
Plate 1

Overland Flow Chart







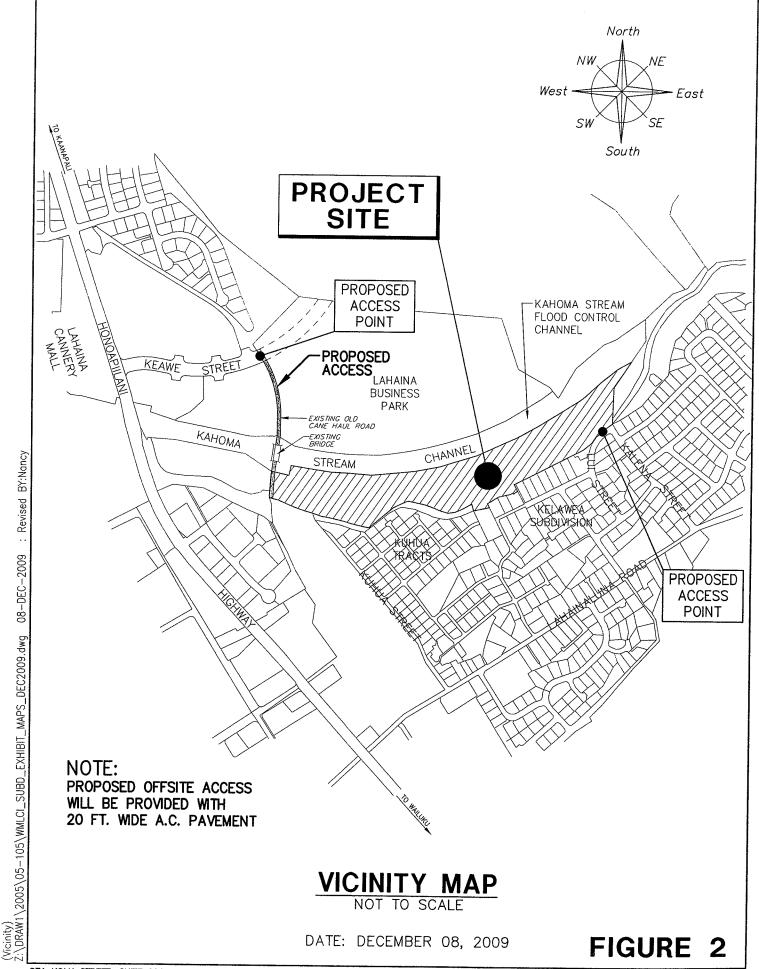




LOCATION MAP ISLAND OF MAUI

FIGURE 1

871 KOLU STREET, SUITE 201 WALLUKU, MAUI, HAWAII 96793 R. T. TANAKA ENGINEERS, INC LAND SURVEYORS - CIVIL & STRUCTURAL ENGINEERS JOB NO. 05-105

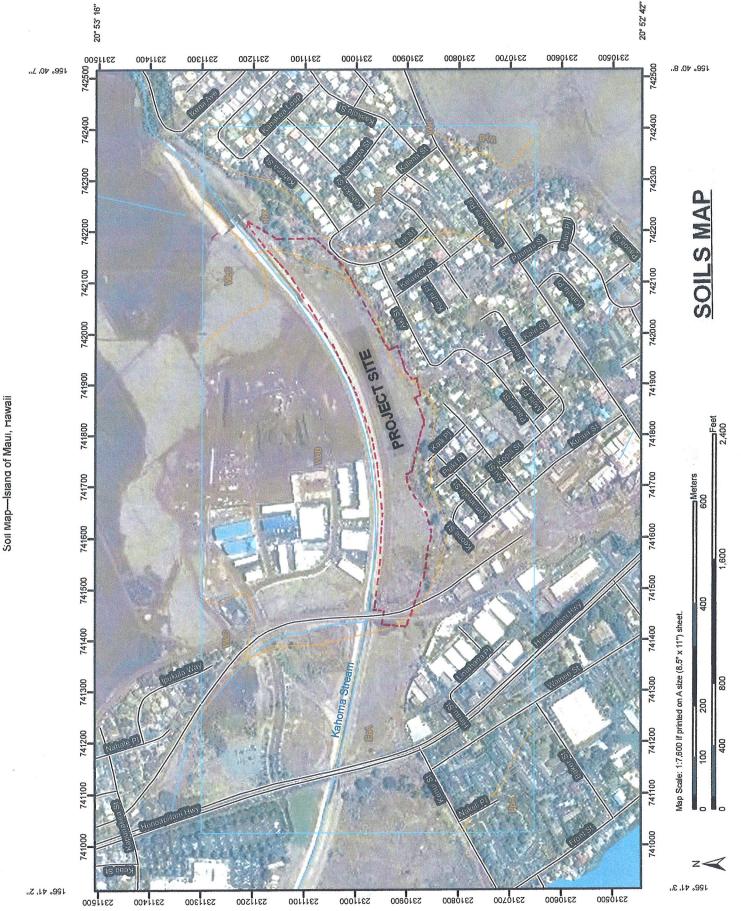


871 KOLU STREET, SUITE 201 WAILUKU, MAUI, HAWAII 96793

R. T. TANAKA ENGINEERS, INC.

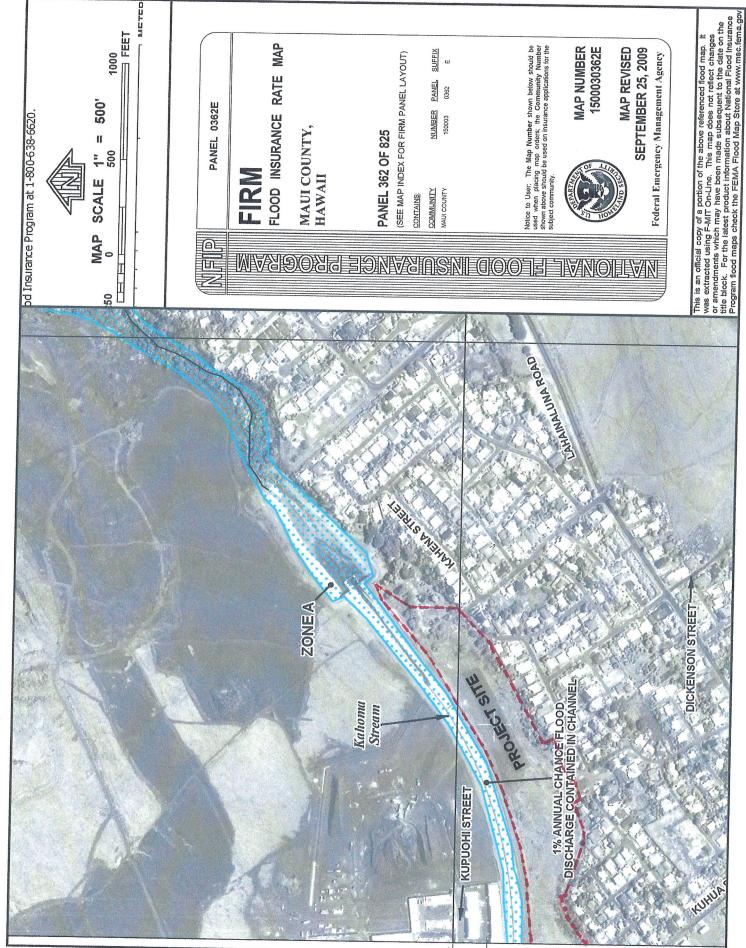
JOB NO. 05-105

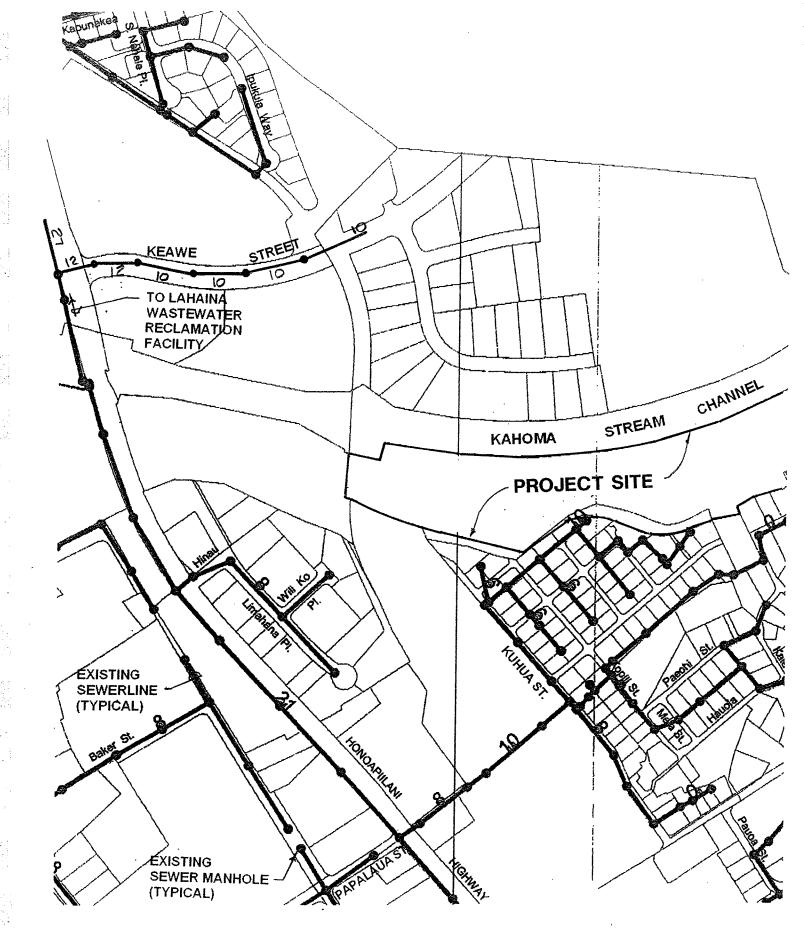
20° 52' 42"



20° 53' 17"

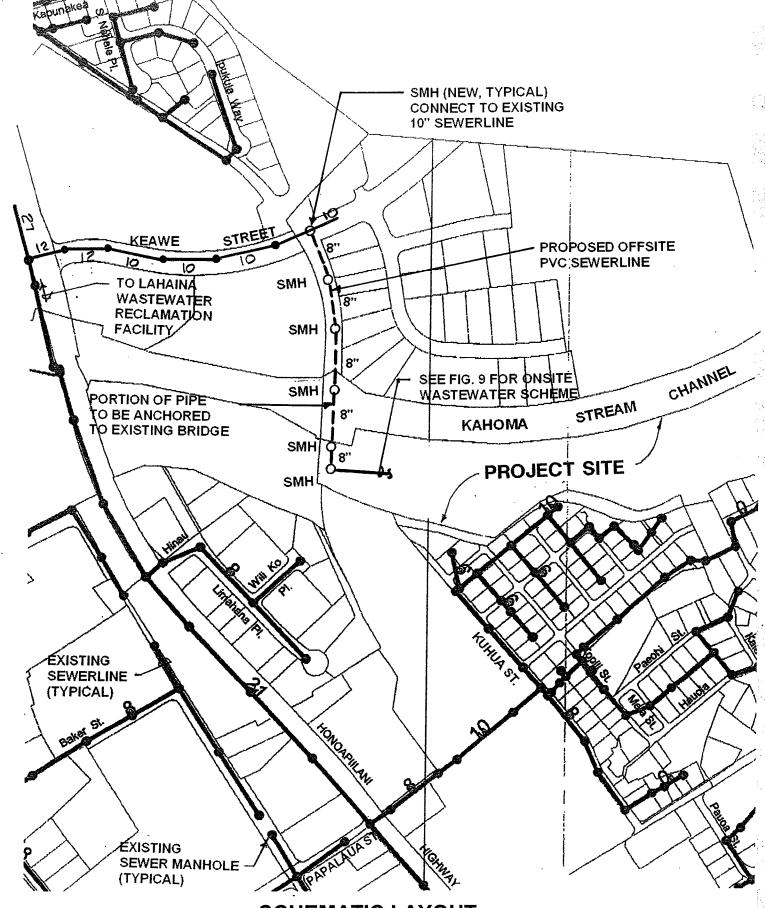
FIGURE 4





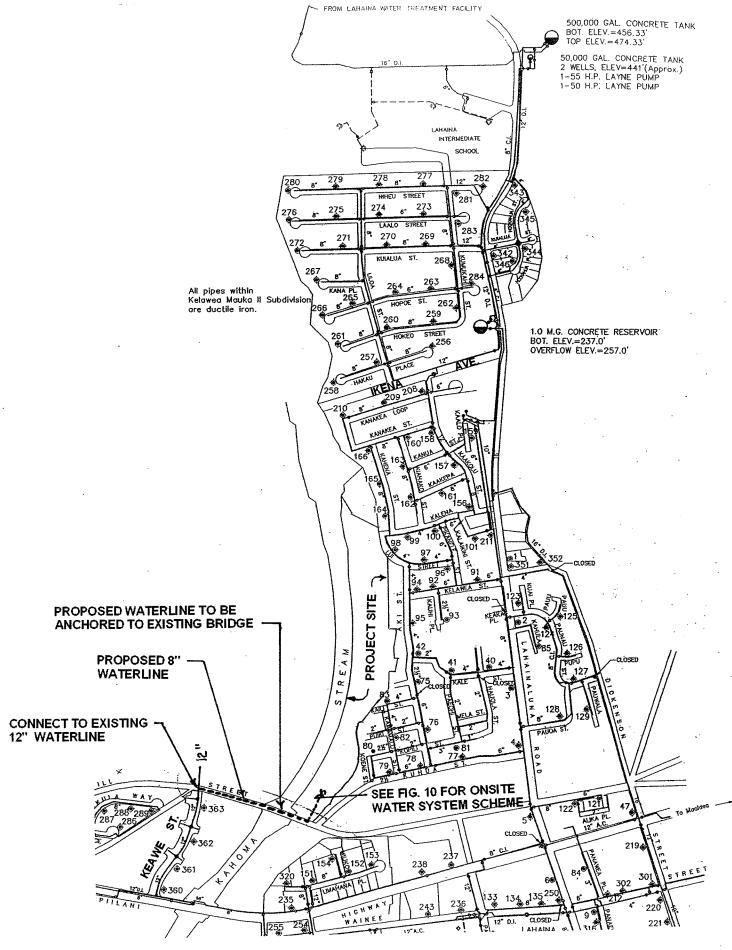
EXISTING COUNTY WASTEWATER SYSTEM

Not to Scale



SCHEMATIC LAYOUT OFFSITE GRAVITY WASTEWATER SYSTEM

Not to Scale



EXISTING COUNTY WATER SYSTEM

Scale: 1" = 800'

